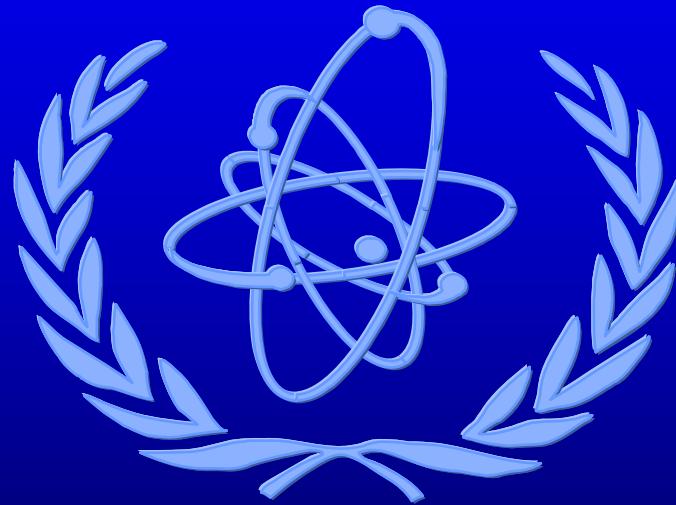


MODULE 3:

**Source Term Phenomena**



# Outline of Discussion

- Review basic fission product release and transport processes
  - Simple calculation methods
  - Major uncertainties
    - Examples from active research
    - Computer code modeling and applications to Level 2 PSA discussed later (M7)
- 



# Fission Product Inventory

- Level of detail needed to define core inventory depends on objective of PSA
  - **Full-scope (Level 3): Complete isotopic inventory**
  - **Typical “IPE” study: concentrate on key radio-elements**
- Computer codes and PSA models work with ‘groups’ of radio-elements
  - **Similar chemical behavior**



# Radionuclide Groups & Typical Inventory

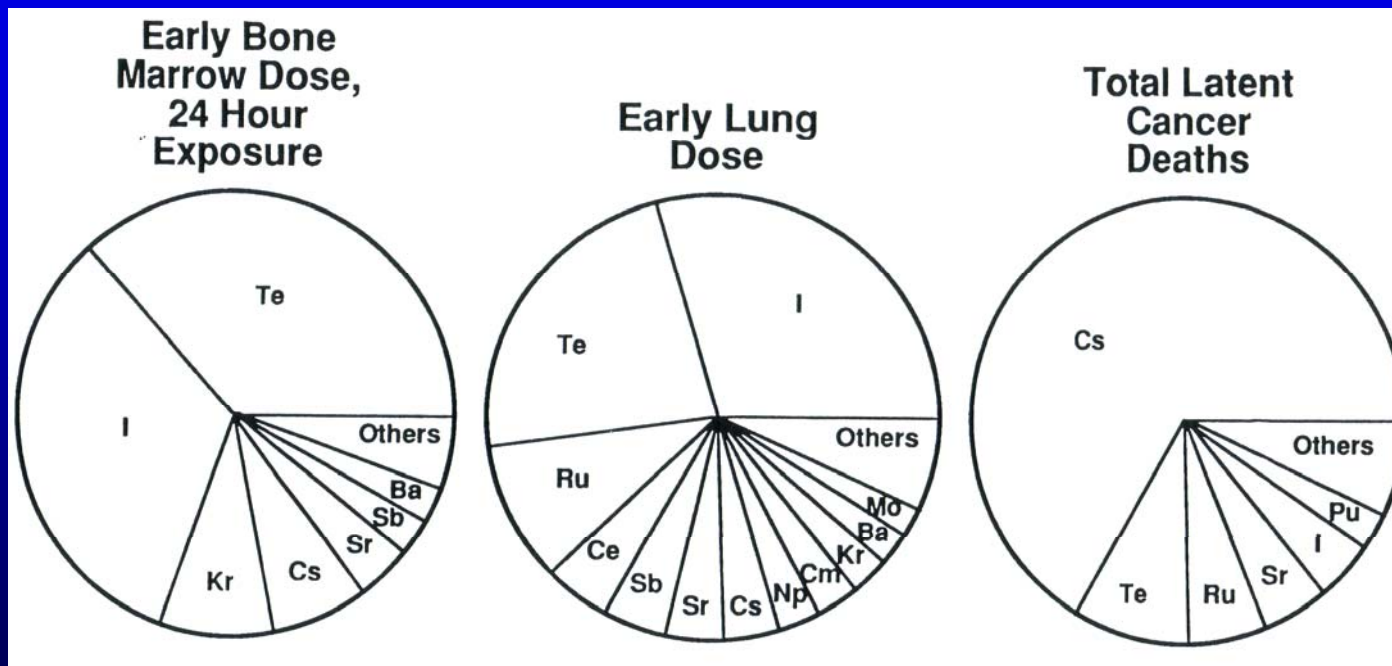
Group No.	Name (representative element)	Elements Contained in Group	End-of-Cycle Mass in Core (kg)
			PWR
1	Noble gases	Xe, Kr	412
2	Iodine	I, Br	18
3	Cesium	Cs, Rb	238
4	Tellurium	Te, Sb, Se	34
5	Strontium	Sr	71
6	Ruthenium	Ru, Rh, Pd, Mo, Tc	612
7	Lanthanum	La, Zr, Nd, Eu, Nb, Pm, Pr, Sm, Y	567
8	Cerium	Ce, Pu, Np	201
9	Barium	Ba	108

Source: AP-600



# Isotopes of Some Elements More Important than Others

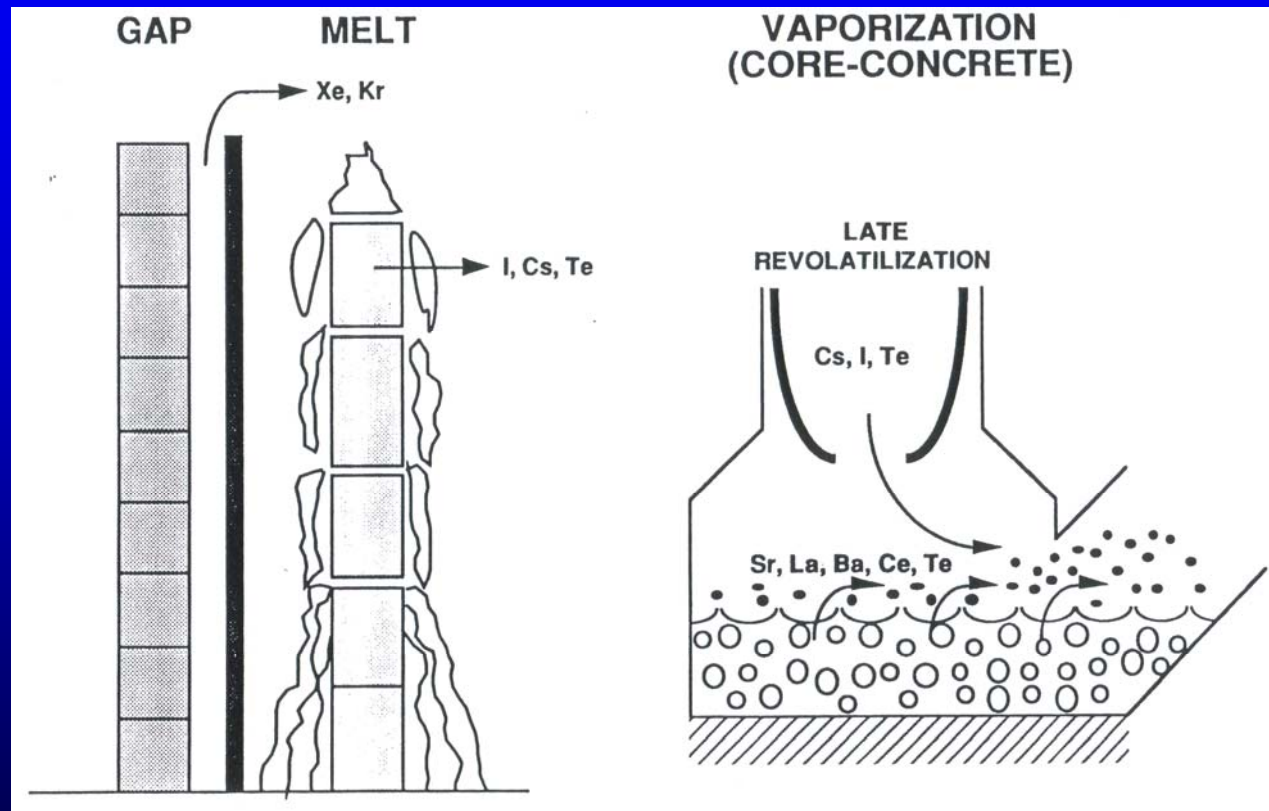
- Relative importance of radio-elements to various human health consequences [Ref: NUREG/CR-4467, U.S. NRC, 1986]



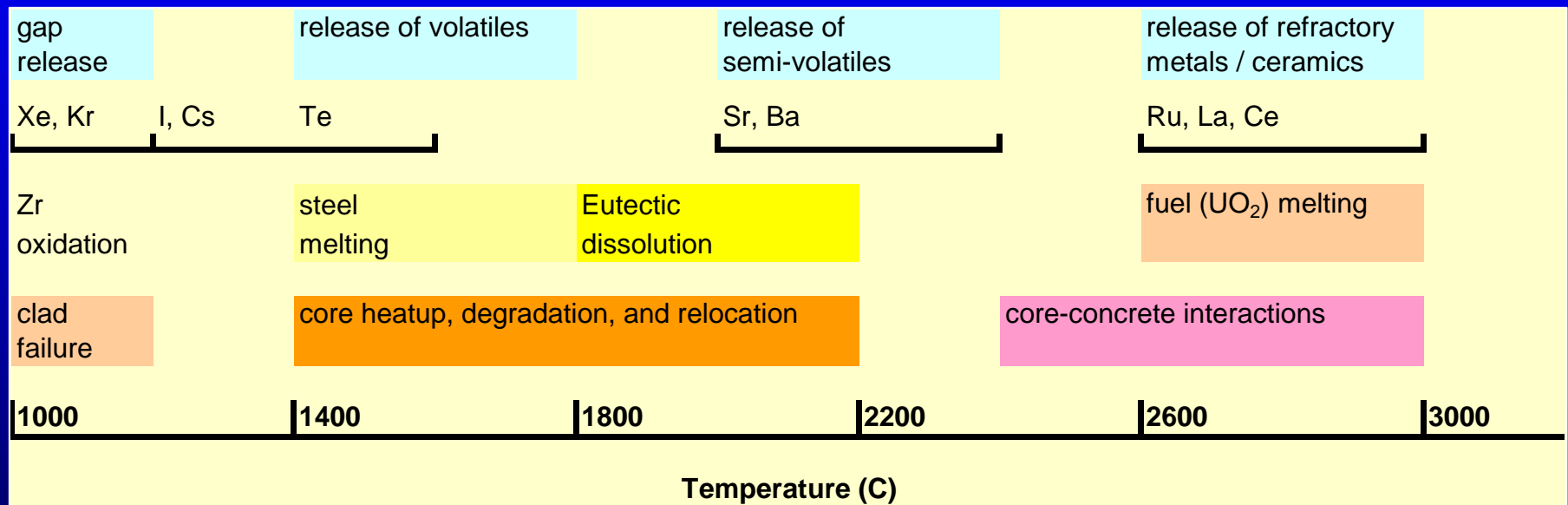
Assumes unit release of each element.



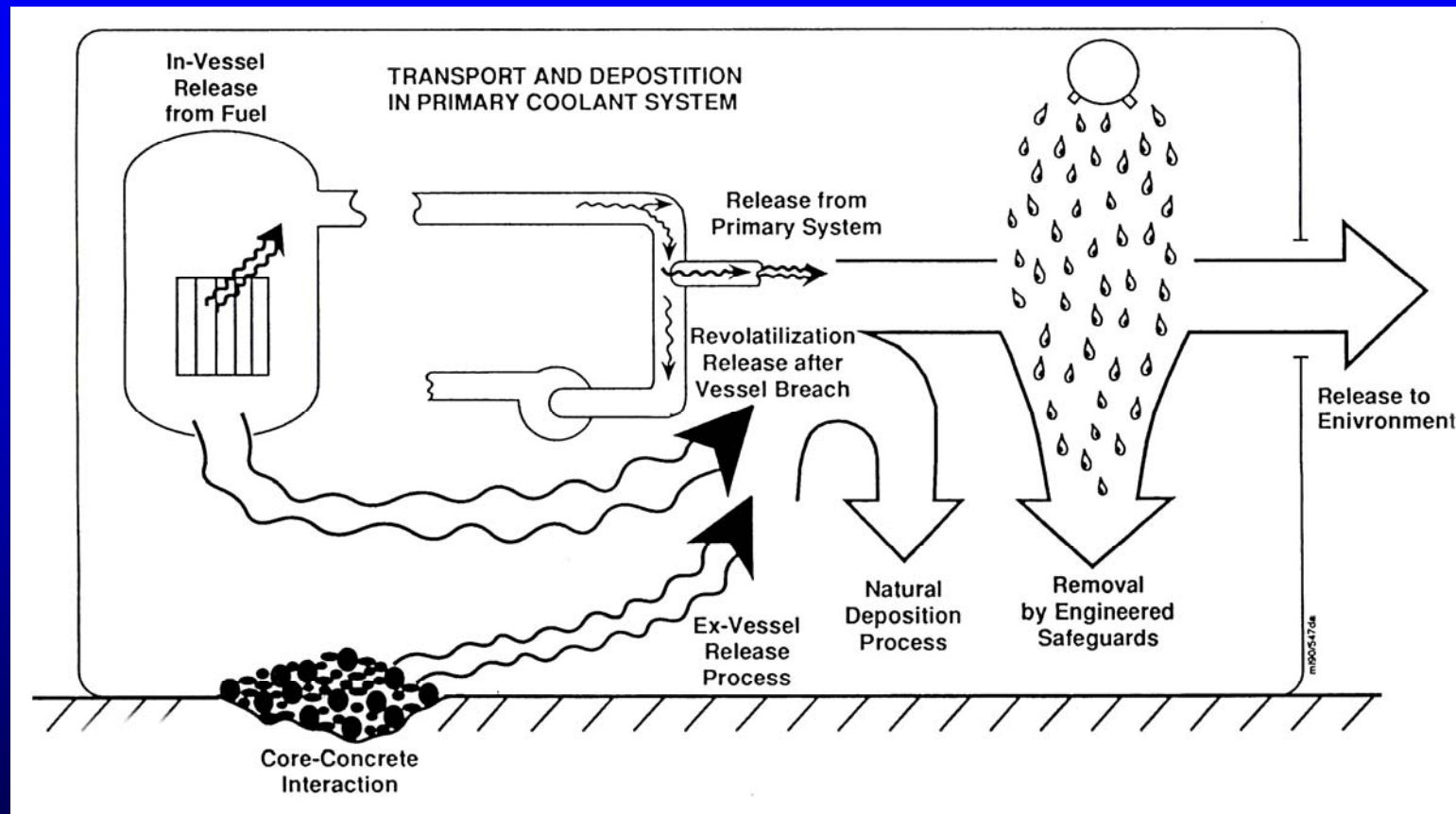
# F.P. Release occurs at Different Times During an Accident



# Fission Product Release a Strong Function of Temperature

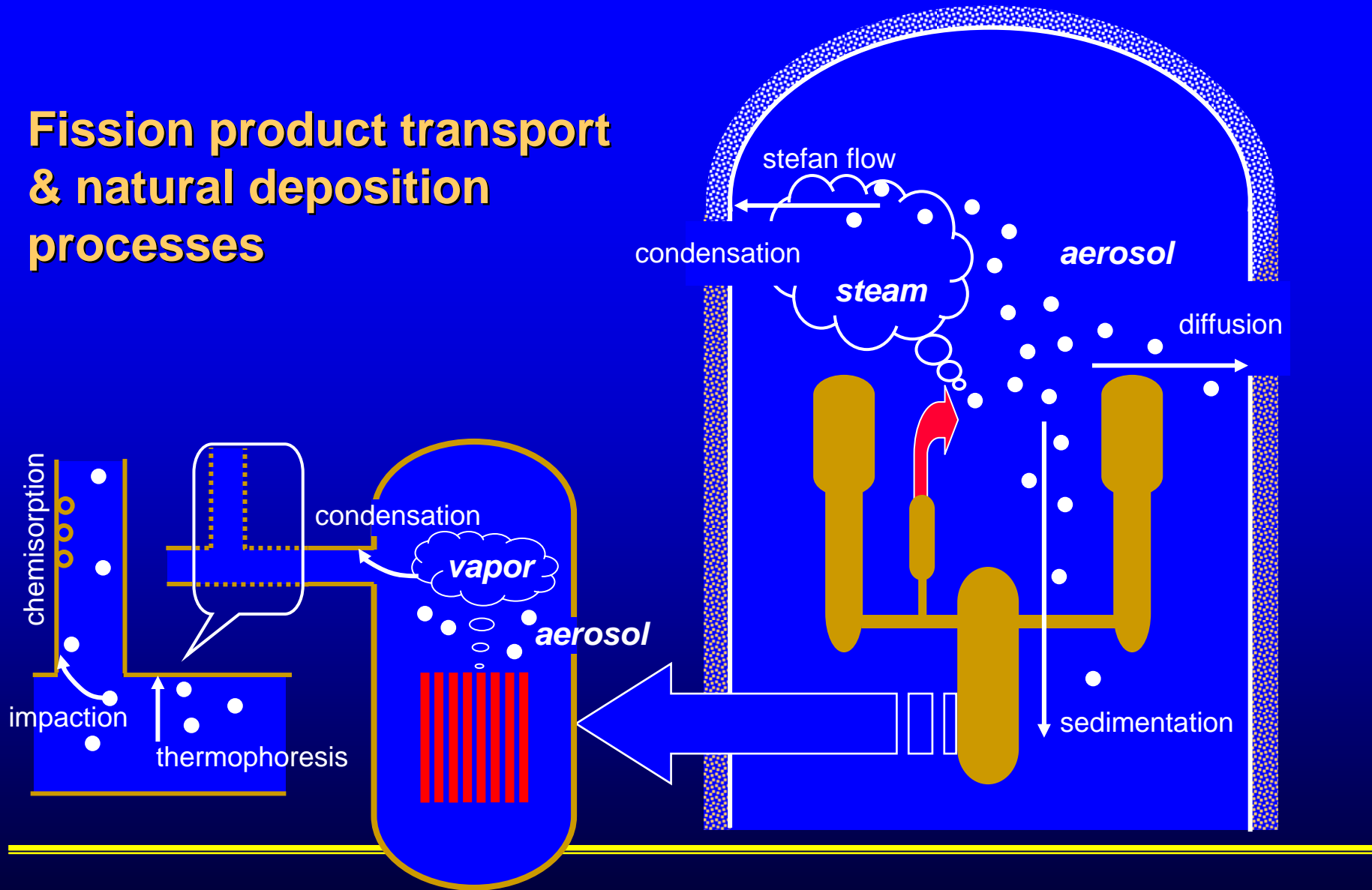


# Deposition Along Transport Path Reduces Inventory Available for Release to Environ.



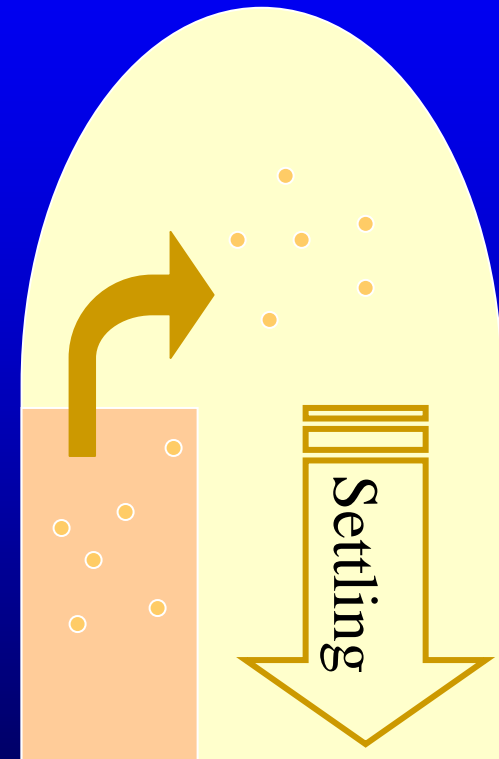


# Fission product transport & natural deposition processes



# Calculation Methods

- Detailed source term assessment requires integrated computer code (discussed later)
- Simpler methods useful to examine broad issues
  - **Gravitational settling (sedimentation) often dominates behavior in containment**
  - **Hand calculations can provide estimates of the importance of deposition in the RCS**

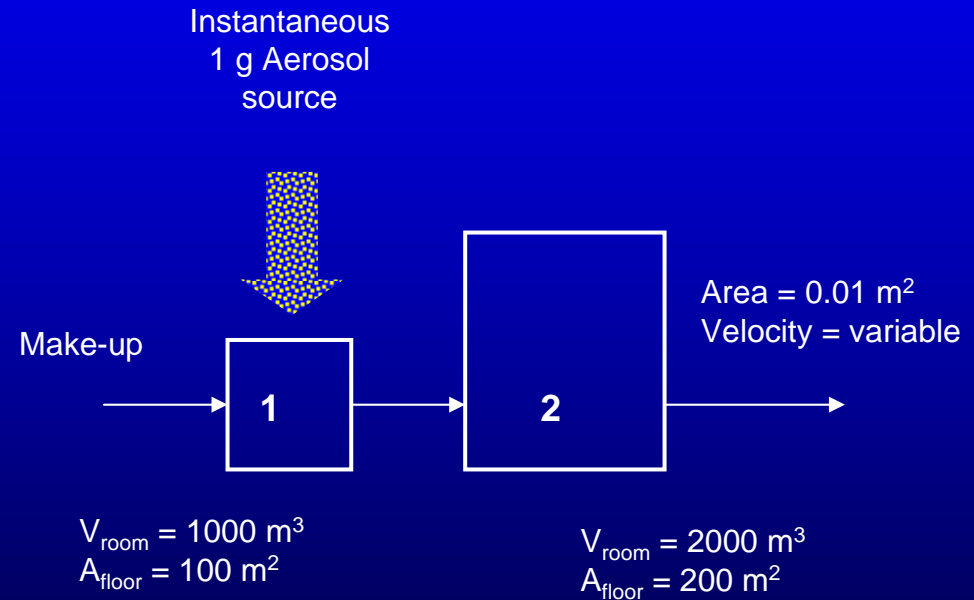
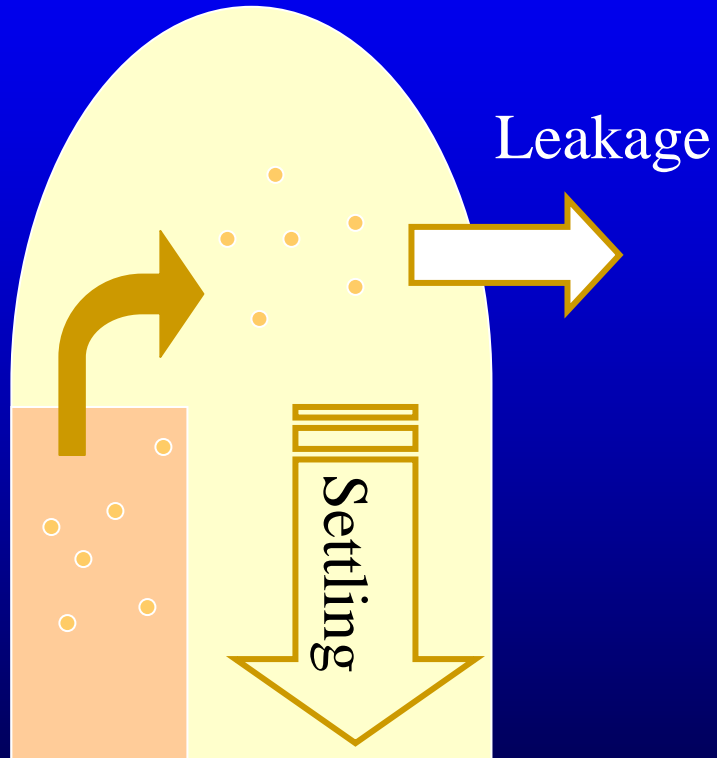


# Two examples of hand-calculations

- Airborne aerosol depletion by gravitational settling
    - Estimate the amount of time needed to reduce airborne concentrations
  - Aerosol deposition on reactor coolant system surfaces at very high temperatures
    - Determine if thermophoresis is important
- 



# Control Volume Approach to Estimating Aerosol Settling Rate



# Control Volume Mass Balance

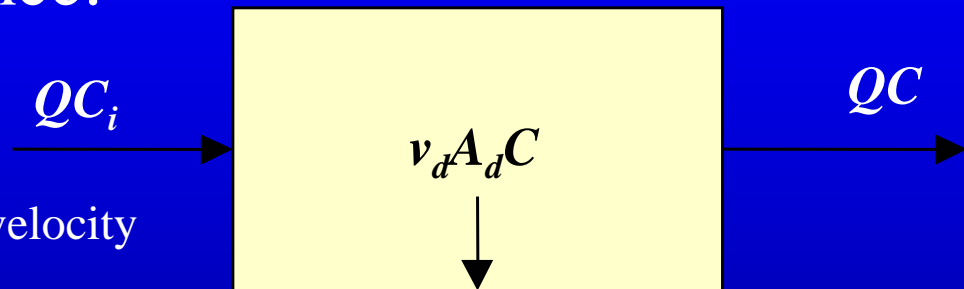
Steady state flow balance:

$Q$  = flow rate

$C$  = particle concentration

$v_d$  = particle deposition (settling) velocity

$A_d$  = deposition (settling) area



$$v_d A_d C = Q (C_i - C)$$

Release Fraction (RF):

$$RF = \left( \frac{QC}{QC_i} \right) = \frac{C}{C_i} = \frac{1}{1 + \frac{v_d A_d}{Q}} = \frac{1}{1 + \alpha}$$



# Deposition by Gravitational Settling

$$v_d = \frac{d_p^2 \rho_p g C_m}{18 \mu \chi}$$

where

$v_d$  = particle settling velocity

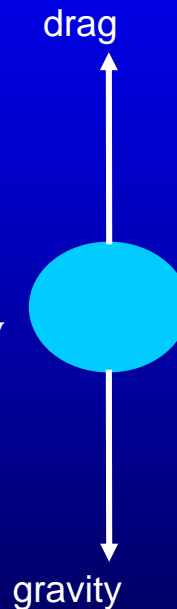
$d_p, \rho_p$  = particle diameter, density

$C_m$  = slip correction factor

$\mu$  = viscosity of air

$\chi$  = dynamic shape factor

Settling (terminal) velocity is proportional the square of particle diameter: ( $v_d \propto d^2$ )



<u>Diameter (<math>\mu\text{m}</math>)</u>	<u>Terminal Velocity (cm/s)</u>
1.0	3.0E-3
2.0	1.2E-2
4.0	4.7E-2
8.0	1.9E-1

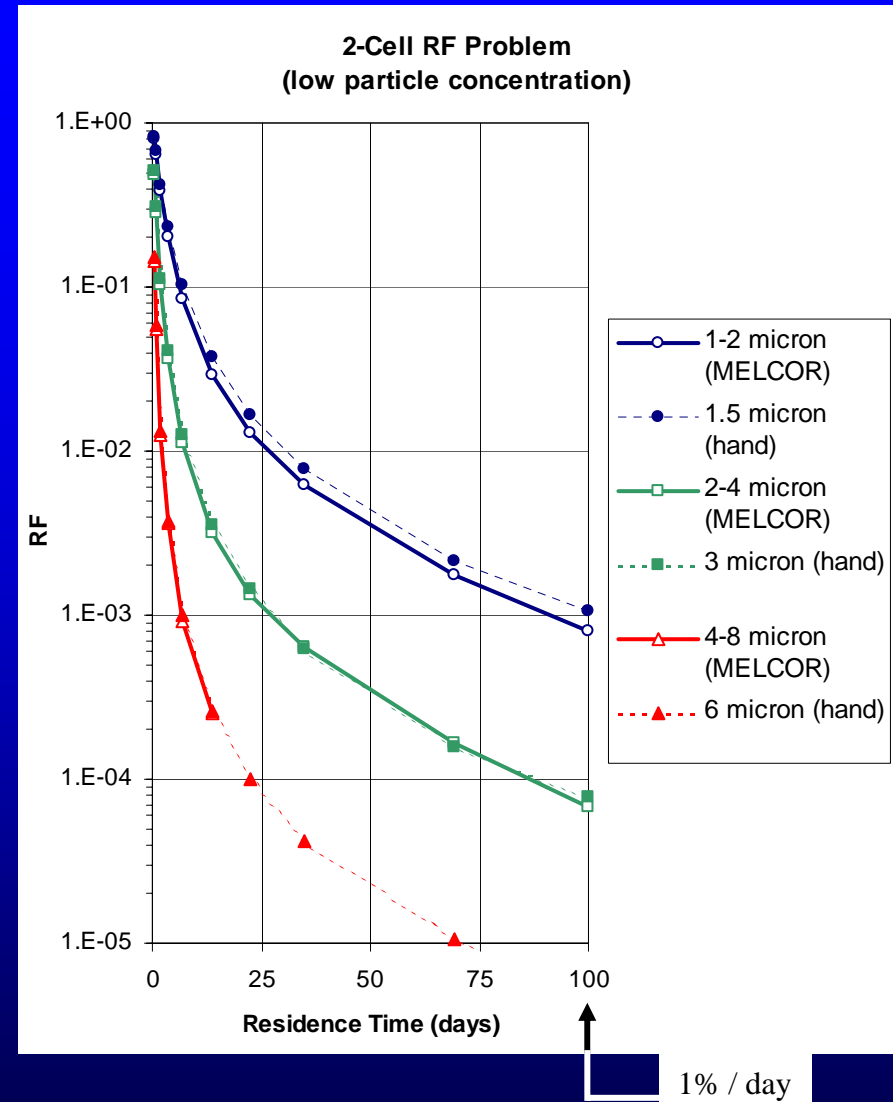


# Results

- Release Fraction (RF) as function of residence time in containment:

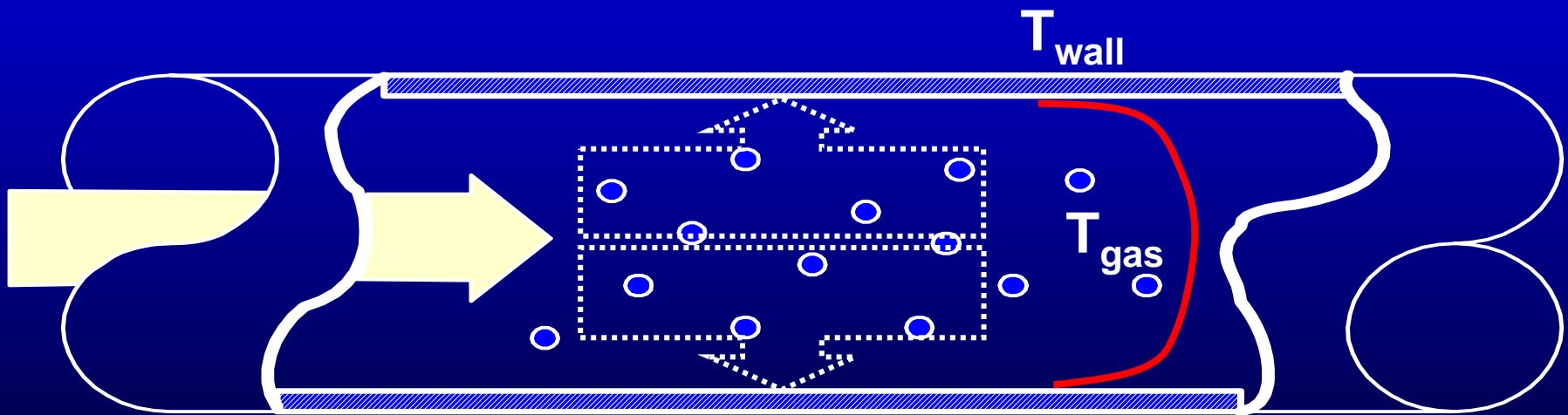
$$Residence\ Time = \frac{Volume}{Leak\ Area * Velocity}$$

- Settling much more efficient for large particles
- Hand calculations for 'simple' problems reproduce code results



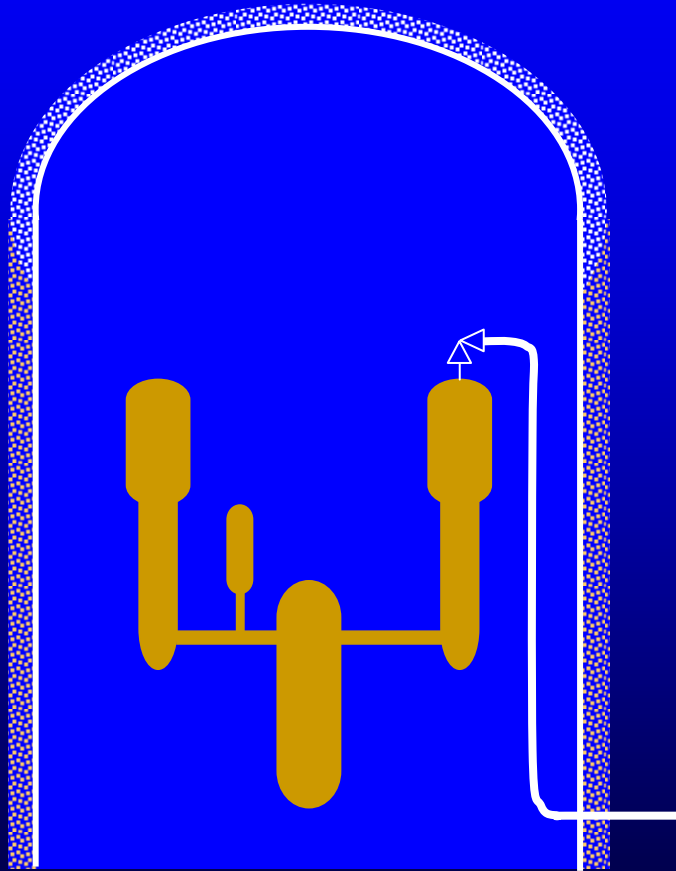
## Example 2: Aerosol Deposition on an RCS Pipe by Thermophoresis

- **Thermophoresis:** movement of an aerosol particle due to a local temperature gradient.
- $dT/dr$  creates a net force from a hot gas toward a cooler surface.





# Estimating Thermophoretic Deposition



- Example: Steam generator relief valve discharge line during a tube-rupture accident sequence
- Objective: Estimate aerosol deposition in the discharge line by thermophoresis
- Gas effluent temperatures (during core damage) can be very high (~900K)
- Pipe wall temperatures may be cooler if valve opens late in time



# Deposition Rate by Thermophoresis

- Rate at which aerosol concentration  $Q$  changes in volume

$V$ :

$$\frac{dQ}{dt} = - \frac{\int |-\bar{v}_t \cdot d\bar{A}|}{V} Q$$

where:  $v_t$  = deposition velocity

$dA$  = surface area normal to  $Q$

Deposition velocity for thermophoresis:

$$v_t = \frac{3\mu C_m (c_t Kn + k_{gas} / k_p) \nabla T}{2\chi \rho_{gas} T (1 + 3 \cdot 1.257 Kn) (1 + 2c_t Kn + k_{gas} / k_p)}$$



## where:

$T$  = pipe temperature,

$\nabla T$  = temperature gradient from the gas to the wall,

$d_p$  = particle diameter,

$c_t$  = constant (2.25),

$g$  = gravitational constant,

$Kn = 2\lambda/d_p$  (Knudsen number),

$k_{gas}/k_p$  = ratio of gas to particle thermal conductivity,

$\lambda$  = mean free path of gas,

$\mu$  = gas viscosity,

$\rho_p$  = particle material density,

$\rho_{gas}$  = gas density, and

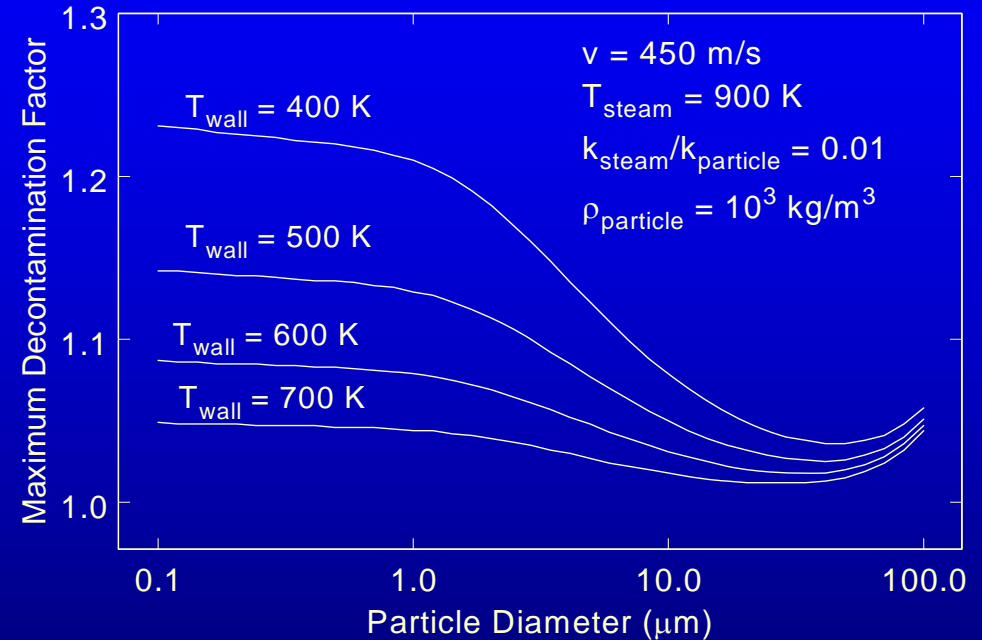
$\chi$  = dynamic shape factor; and

$$C_m = 1 + \frac{2\lambda}{d_p} [1.257 + 0.4 \exp(-0.55d_p / \lambda)]$$



## Results for sample SGTR RV discharge line deposition

- Assume  $T_{\text{gas}}$  in the pipe  $\sim 900\text{K}$
- $T_{\text{wall}}$  is a function of time spanning range of  $400\text{K}$  to  $700\text{K}$
- Gas velocities near sonic ( $\sim 450\text{ m/s}$ )



Result: Deposition significant only for:  
Very small aerosols and  $\Delta T > 300^\circ\text{C}$



## Simplified methods -- summary

- Simple, “hand” calculations provide useful information on
    - **the time-scale for major deposition mechanisms to operate, and**
    - **the importance of deposition mechanisms under specific conditions.**
  - A summary of simplified source term estimation methods can be found in: IAEA-TECDOC-1127.
  - BUT -- Simple calculations can not completely replace fully-integrated computer codes calculations of accident source terms
    - **However, they help define the level of detail required in modeling plant behavior**
- 



# Source Term Uncertainties

- Focus of Recent Research -

- Chemical form of iodine
  - Phase and chemical transformations occur in containment atmosphere and aqueous solutions
  - Leads to late re-evolution of iodine from pools of water
- Chemical reactions with cesium in the RCS
  - CsI reaction well established
  - Recent evidence from PHEBUS suggests additional reactions with molybdenum ( $\text{Cs} \rightarrow \text{Cs}_2\text{MoO}_4$ )
  - Challenging historical assumption that most cesium is transported as an oxide ( $\text{CsOH}$ )



- Published validation of source term computer code models for these effects is very limited

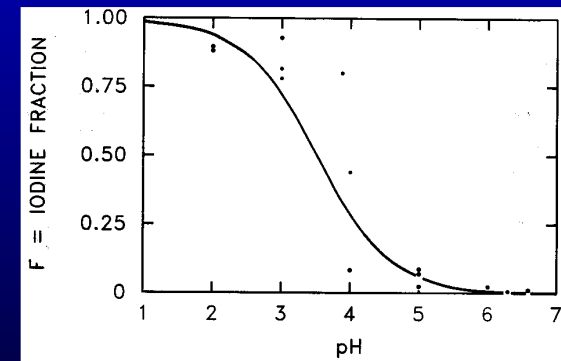
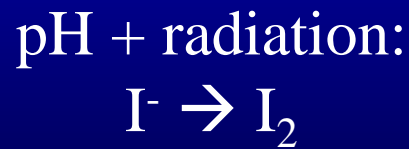
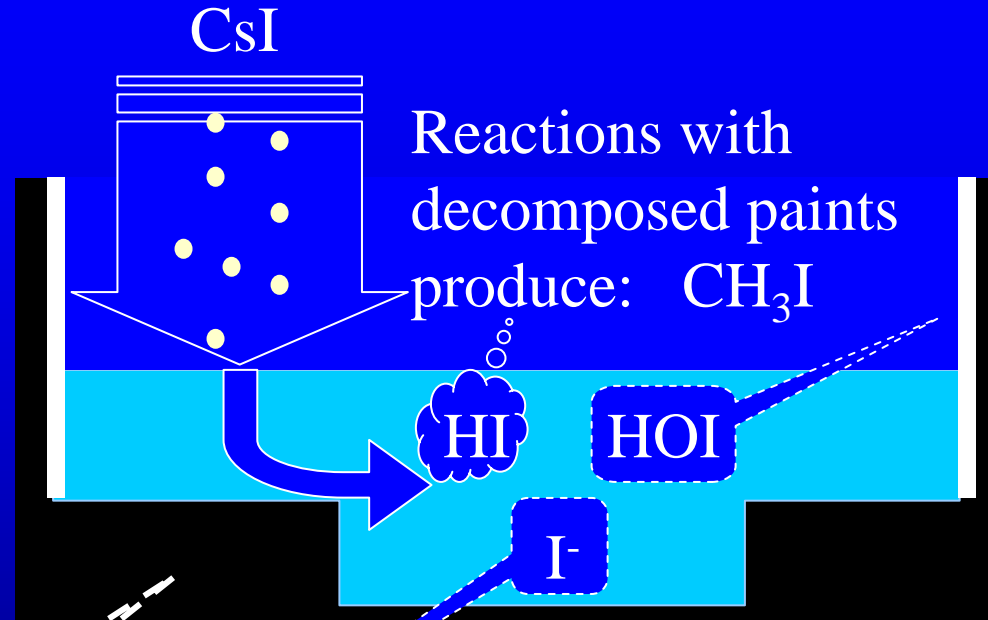
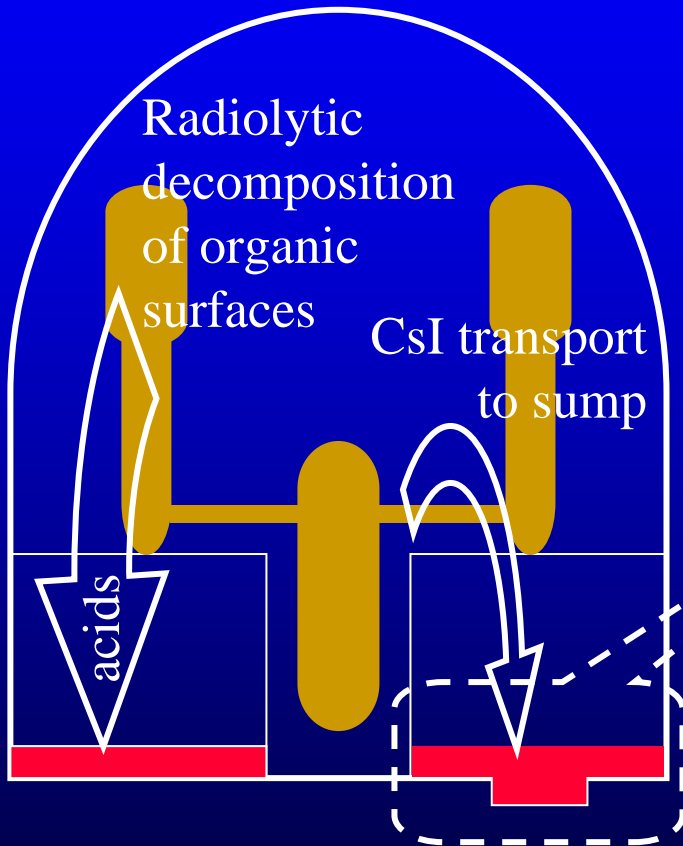


# Iodine Behavior in Containment

- Cesium iodide (CsI) is the dominant form of iodine transported to containment
  - CsI is highly soluble
    - **Tendency to collect in pools of water**
  - Chemical and radiolytic environment enhances reactions that yields volatile forms of iodine
    - **Effect is to increase long-term release to environment**
- 



# Iodine Chemistry



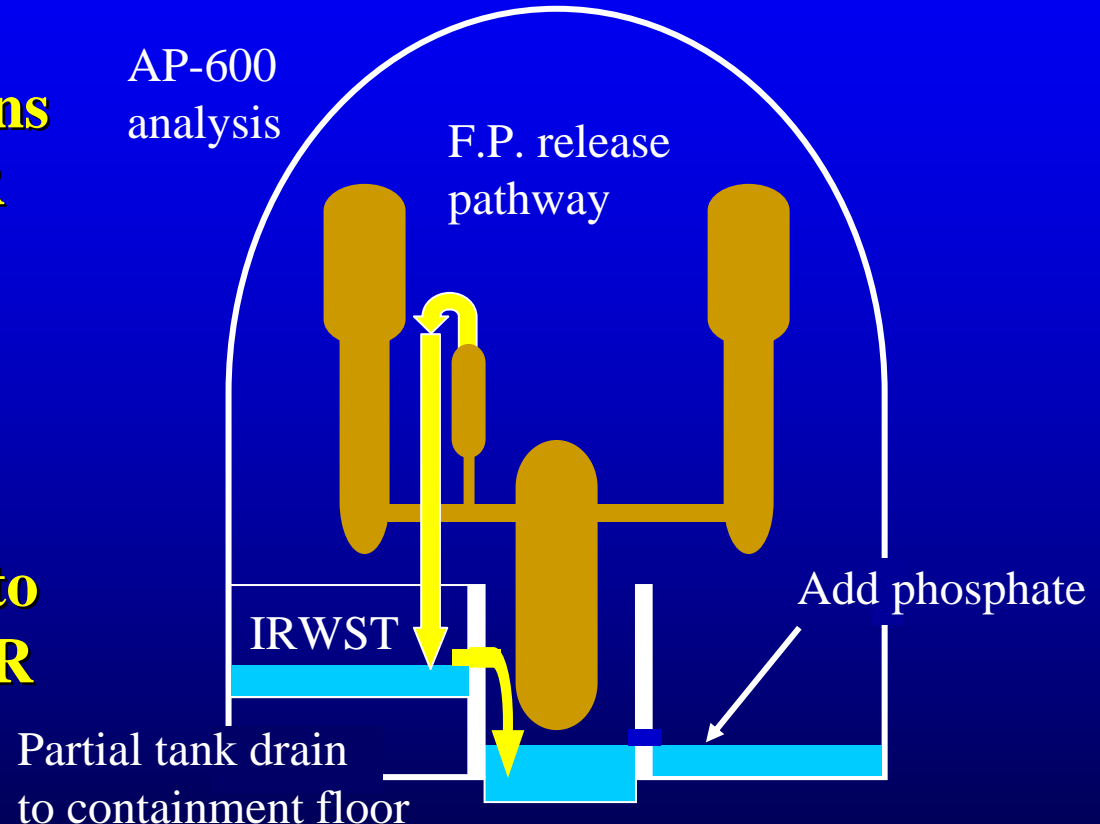


# Example Calculation of Long-term Iodine Release

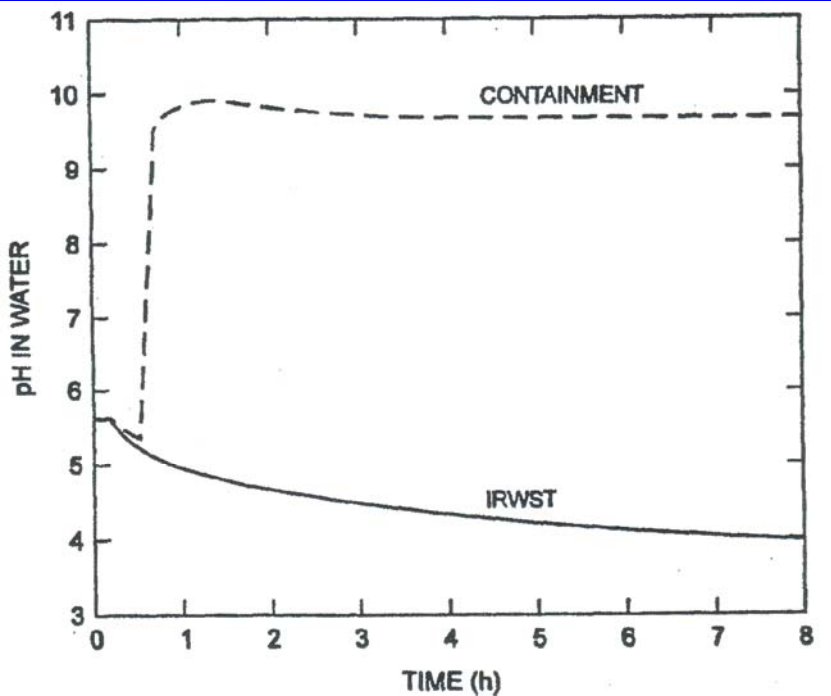
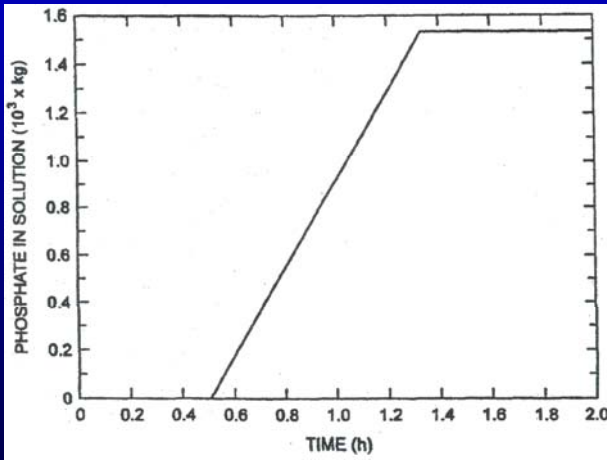
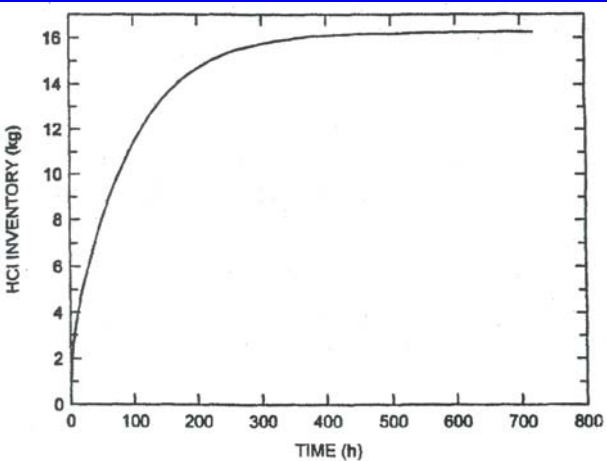
- **Detailed calculations of chemical transformations for representative PWR and BWR**

- Evaluate needs for post-accident pH control

- **Models recently added to TRENDS and MELCOR codes**



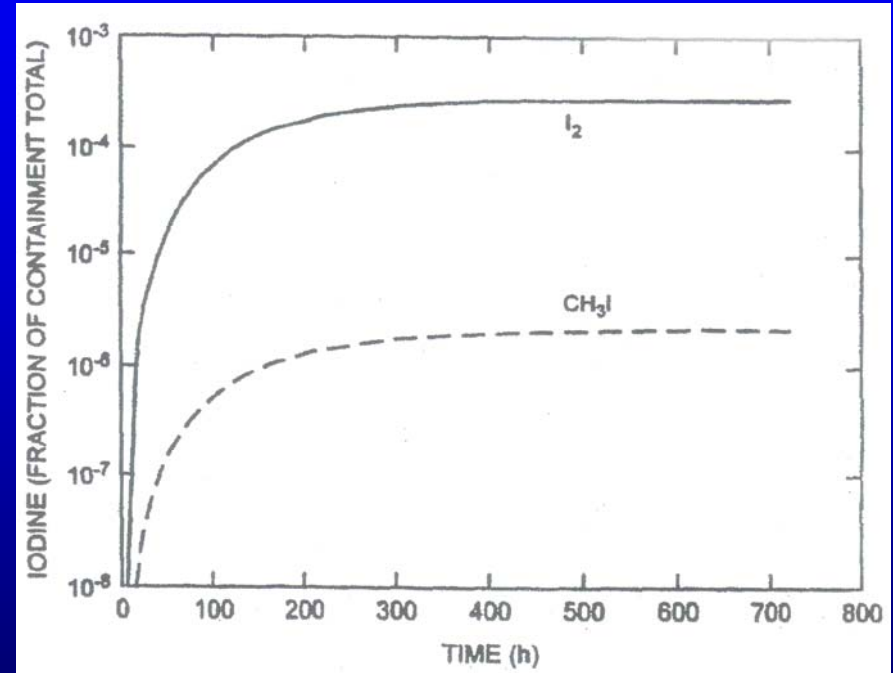
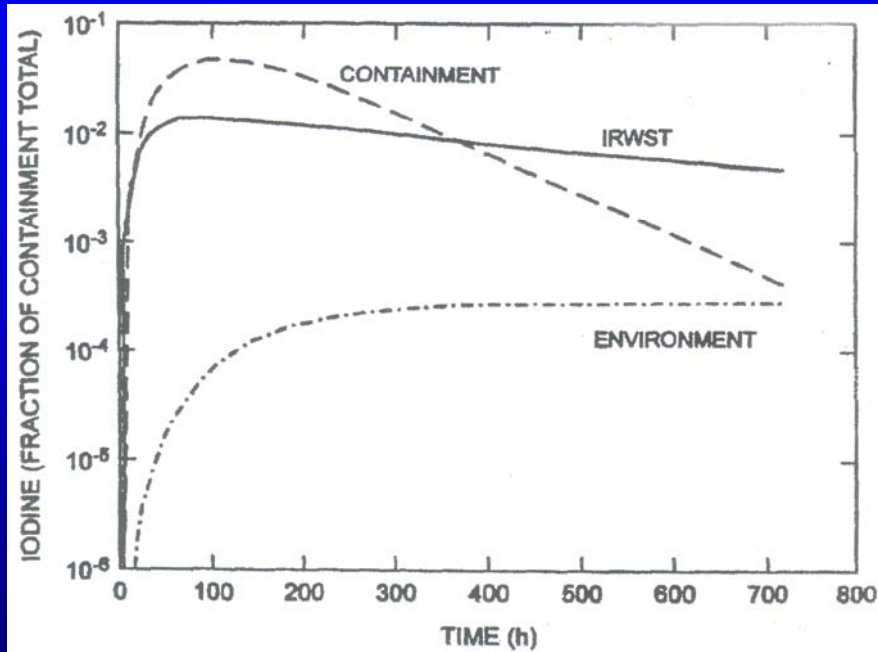
# Example Calculation: AP-600



Ref: TRENDS analysis in NUREG/CR-6599, Oct 1998



# AP-600 example (2)



Ref: NUREG/CR-6599, Oct 1998



## Source Term Phenomena:

# Summary

- **Dominant phenomena for fission product release & transport have substantial data base to support code calculations**
    - **Well established models exist for fission product release from fuel, aerosol growth and major deposition processes**
    - **Simple calculation methods are useful for first-order evaluations of major issues**
    - **Fully-integrated, computer simulations are necessary for a comprehensive source term assessment**
  - **Substantial uncertainties remain**
    - **Must account for code modeling limitations in defining source terms for Level 2 PSA**
- 
- 

